

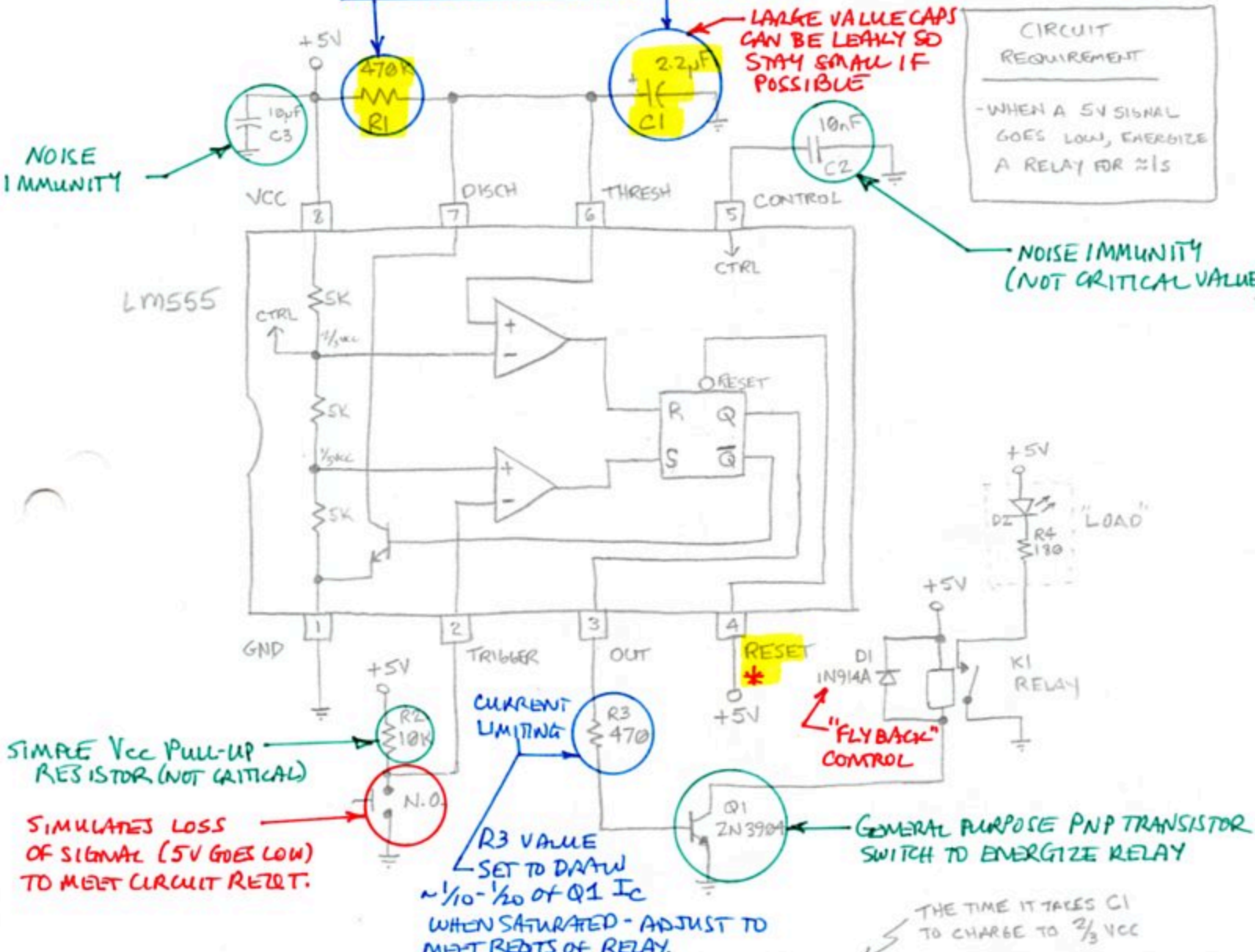
BACK TO BASICS

555 BASED "ONE-SHOT"

MONOSTABLE MULTIVIBRATOR

- OUTPUTS A SINGLE PULSE IN RESPONSE TO A TRIGGER

R1, C DETERMINE PULSE WIDTH OUTPUT



**CIRCUIT REQUIREMENT**  
 - WHEN A 5V SIGNAL GOES LOW, ENERGIZE A RELAY FOR  $\approx 1$ S

NOISE IMMUNITY

NOISE IMMUNITY (NOT CRITICAL VALUE)

SIMPLE Vcc PULL-UP RESISTOR (NOT CRITICAL)

SIMULATES LOSS OF SIGNAL (5V GOES LOW) TO MEET CIRCUIT REQT.

CURRENT LIMITING  
 R3 VALUE - SET TO DATA SHEET  
 $\sim 1/10 - 1/20$  of Q1 Ic  
 WHEN SATURATED - ADJUST TO MEET REQS OF RELAY.

GENERAL PURPOSE PNP TRANSISTOR SWITCH TO ENERGIZE RELAY

"FLYBACK" CONTROL

- PULSE "ON" TIME IS:  $t_{ON} = 1.1 * R1 * C1$

\* RESET LINE TIED TO 5V SINCE WE'RE NOT USING THAT FUNCTION

REMEMBER, A SIMPLE RC CIRCUIT CHARGES TO 63% IN ONE RC TIME CONSTANT. HERE, WE WANT 66.7%, SO IT MAKES SENSE THAT THE TIME IS JUST OVER 1 RC

THE TIME IT TAKES C1 TO CHARGE TO  $2/3$  VCC

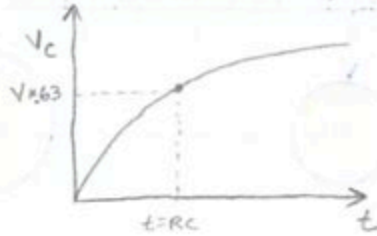
# BACK TO BASICS

W2AEW

## 555 ONE-SHOT MATH

WHY IS THE TIME =  $1.1 * RC$

FOR RC CIRCUIT  
(CHARGING)



$$V_c(t) = V * (1 - e^{-t/RC})$$

RE-ARRANGE TO SOLVE FOR t

DIVIDE BY V:

$$\frac{V_c(t)}{V} = 1 - e^{-t/RC}$$

SUBTRACT/SWAP:

$$e^{-t/RC} = 1 - \frac{V_c}{V}$$

NATURAL LOG :

$$\frac{-t}{RC} = \ln\left(1 - \frac{V_c}{V}\right)$$

MULTIPLY BY -RC:

$$t = -RC * \ln\left(1 - \frac{V_c}{V}\right)$$

IN OUR CASE,  $\frac{V_c}{V} = \frac{2}{3}$

THUS

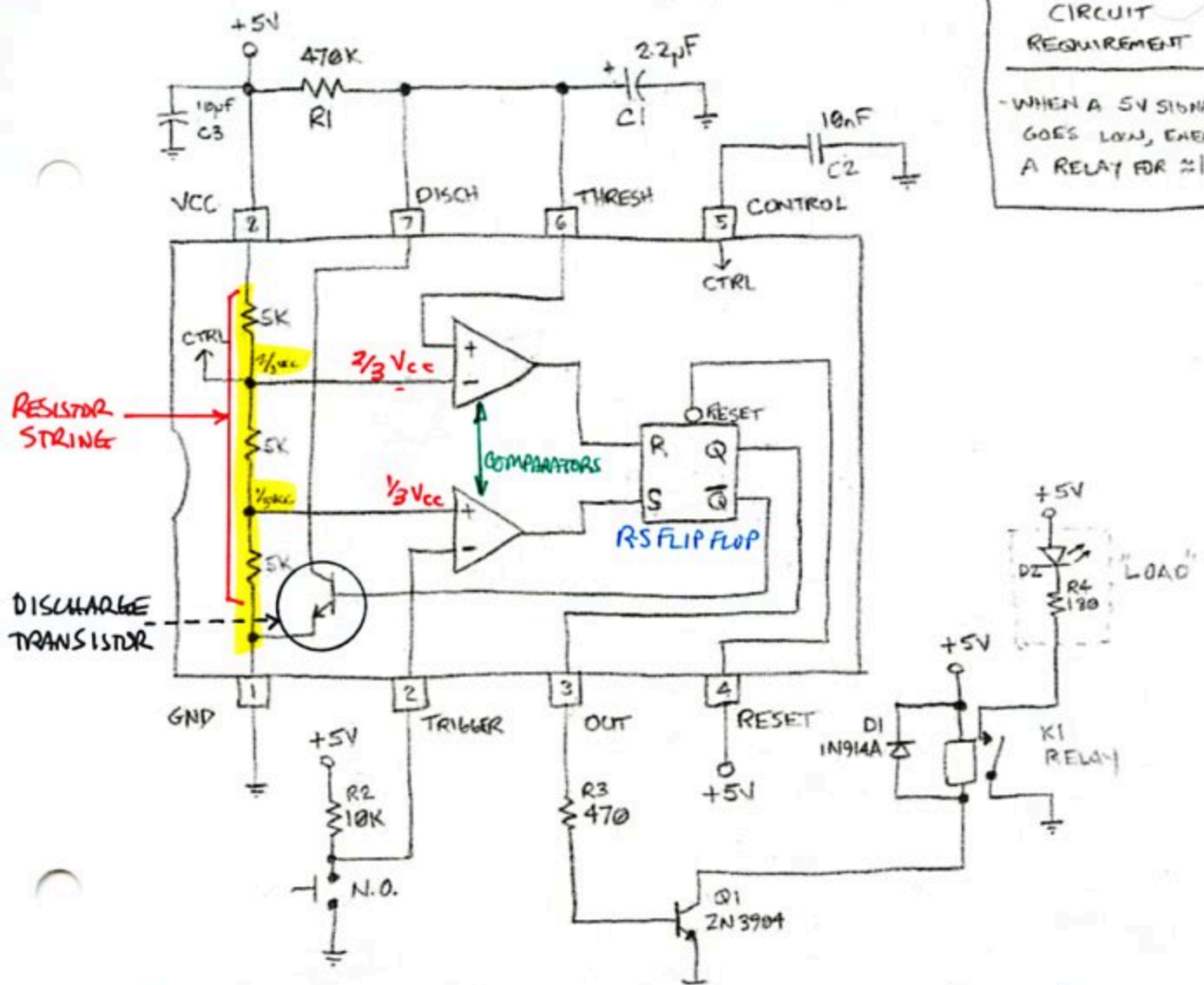
$$t = -RC * \ln\left(1 - \frac{2}{3}\right)$$

$$t = -RC * \ln\left(\frac{1}{3}\right)$$

$$t = 1.1 * RC$$

CIRCUIT REQUIREMENT

- WHEN A 5V SIGNAL GOES LOW, ENERGIZE A RELAY FOR ~1S



- 1 RESISTOR STRING SETS UP A VOLTAGE DIVIDER PRESENTING  $\frac{2}{3}$  AND  $\frac{1}{3}$   $V_{CC}$  AT THE INPUTS OF THE TWO COMPARATORS
- 2 AT POWER UP THE R-S FLIP FLOP IS IN A RESET CONDITION
  - "Q" OUTPUT IS LOW  $\therefore$  Q1 IS OFF AND LOAD (RELAY) IS NOT ENERGIZED
  - "Q-bar" OUTPUT IS HIGH  $\therefore$  THE TRANSISTOR AT THE BOTTOM OF THE RESISTOR STRING IS TURNED ON AND IS PULLING CURRENT DOWN THRU R1 VIA THE "DISCH" PIN #7 PIN WHICH SATURATES THE TRANSISTOR AND PREVENTING C1 FROM CHARGING UP. THIS MEANS THE VOLTAGE AT PIN#6 "THRESH" REMAINS LOW (NEAR GND)  $\rightarrow$  THUS THE OUTPUT OF THE TOP COMPARATOR IS LOW AND WE'RE NOT GOING TO RESET THE FLIP FLOP ("R").
- 3 WITH 5V APPLIED TO THE TRIGGER (PIN#2) INPUT THE OUTPUT OF THE LOWER COMPARATOR IS ALSO LOW  $\therefore$  THE FLIP FLOP WILL NOT CHANGE STATE.
- 4 IF THE TRIGGER VOLTAGE (PIN#2) IS BROUGHT BELOW  $\frac{1}{3}$   $V_{CC}$  THE OUTPUT OF THE LOWER COMPARATOR GOES HIGH  $\rightarrow$  DO THIS BY PRESSING THE SWITCH (N.O.) TO BRING PIN#2 TO GND (AND  $< \frac{1}{3}$   $V_{CC}$ ).
- 5 THE FLIP FLOP OUTPUT THEN GOES HIGH, IN TURN CAUSING Q1 TO TURN ON AND THE RELAY, AS WELL.
- 6 AT THE SAME TIME "Q-bar" GOES LOW TURNING OFF THE DISCHARGE TRANSISTOR AT THE BOTTOM OF RESISTOR STRING BRINGING THE "DISCH" PIN (PIN#7) TO ESSENTIALLY OPEN CIRCUIT NOW ALLOWING C1 TO CHARGE UP THRU R1; IT CHARGES EXPONENTIALLY.

- ▲ C1 CHARGES EXPONENTIALLY UNTIL IT REACHES  $\frac{2}{3}$  of  $V_{cc}$  AT WHICH POINT THE TOP COMPARATOR GOES HIGH AND RESETS THE FLIP FLOP.
- ▲ AS SOON AS THE FLIP FLOP RESETS "Q" OUTPUT GOES LOW THUS TURNING Q1 OFF AGAIN WHICH TURNS OFF THE RELAY AGAIN.
- ▲ "Q" GOES HIGH AT THE SAME TIME THUS TURNING ON THE DISCHARGE TRANSISTOR AND QUICKLY TAKES THE CHARGE OFF C1 BRINGING THAT POINT BACK TO THE SATURATION VOLTAGE OF THE TRANSISTOR.
- ▲ WE'RE NOW READY FOR THE NEXT TRIGGER EVENT.
- ▲ NOTE THAT  $t_{on}$  IS A LITTLE BIGGER THAN THE PRODUCT OF  $R1 \times C1$  SINCE THE R-C CIRCUIT ONLY CHARGES TO 63% IN ONE TIME CONSTANT SO WE'RE MAKING SURE IT'S ON LONG ENOUGH TO BRING THE  $\frac{2}{3} V_{cc}$  POINT ON THE TOP COMPARATOR'S INPUT TO ITS FULL VALUE; SO WE USE A MULTIPLICATION FACTOR OF  $\times 1.1$  TO ENSURE IT DOES.

\* NOTE: ONCE THE CIRCUIT IS TRIGGERED IT WON'T BE AVAILABLE TO RE-TRIGGER UNTIL IT RESETS. DEMONSTRATE THIS BY TRIGGERING QUICKLY THE TRIGGER PIN (COULD BE SWITCH BOUNCE)

